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Original Citation

Dhimish, Mahmoud, Holmes, Violeta, Mehrdadi, Bruce and Dales, Mark (2017) The impact of cracks on photovoltaic power performance. Journal of Science: Advanced Materials and Devices, 2 (2). pp. 199-209. ISSN 2468-2179

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The impact of cracks on photovoltaic power performance

Mahmoud Dhimish¹, Violeta Holmes, Bruce Mehrdadi, Mark Dales

Department of Computing and Engineering, University of Huddersfield, Huddersfield, United Kingdom

1. Introduction

Cell cracks appear in the photovoltaic (PV) panels during their transportation from the factory to the place of installation. Also, some climate proceedings such as snow loads, strong winds and hailstorms might create some major cracks on the PV modules surface [1–3]. These cracks may lead to disconnection of cell parts and, therefore, to a loss in the total power generated by the PV modules [4].

There are several types of cracks that might occur in PV modules: diagonal cracks, parallel to busbars crack, perpendicular to busbars crack and multiple directions crack. Diagonal cracks and multiple directions cracks always show a significant reduction in the PV output power [5].

Moreover, the PV industry has reacted to the in-line non-destructive cracks by developing new techniques of crack detection such as resonance ultrasonic vibration (RUV) for screening PV cells with pre-existing cracks [6]. This helped reduce cell cracking due to defective wafers, but, it does not mitigate the cracks generated during the manufacturing process of PV modules.

When cracks appear in a solar cell, the parts separated from the cell might not be totally disconnected, but the series resistance across the crack varies as a function of the distance between the cell parts and the number of cycles for which module is deformed [7]. However, when a cell part is fully isolated, the current decrease is proportional to the disconnected area [8,9].

Collecting the data from damaged PV modules using installed systems is a challenging task. Electroluminescence (EL) imaging method is used to scan the surface of the PV modules, the light output increases with the local voltage so that regions with poor contact show up as dark spots [10,11]. The thermography technique is simpler to implement, but the accuracy of the image is lower than that of the EL technique and does not allow for estimation of the area (in mm²) that is broken in the solar cells [12,13]. Therefore, in this paper we have used the EL imaging method which has been illustrated and discussed briefly in previous works [14–16].

As proposed in [2], the performance of PV systems can be monitored using virtual instrumentation software such as LabVIEW. Also MATLAB software allows users to create tools to model, monitor and estimate the performance of photovoltaic systems. The simulation tool is important to compare the output measured data from PV module with its own theoretical performance [17].

There are a few statistical analysis tools that have been deployed in PV applications. The commonly used tool is the normal standard deviation limits (±1 SD or ± 3 SD) technique [18]. However, a statistical local distribution analysis has been used in identifying the type of cracks in PV modules [5]. To the best of our knowledge, only a few of the previous studies have used a real-time long-term statistical analysis approach for PV cracked modules under real-time operational process. Therefore, the main contribution of this work can be illustrated as follows:
Development of a novel statistical analysis approach that can be used to identify significant effect of cracks on the output power performance for PV modules under various environmental field data measurements.

• Proving that not all cracks have a significant impact on the PV output power performance.

This paper is organized as follows: Section 2 describes the methodology used which contains the data acquisition, PV modules cracks and the statistical analysis approach, while Section 3 lists the output results of the entire work. The discussion is presented in Section 4. Finally, Sections 5 and 6 describe the conclusion and the acknowledgment respectively.

2. Methodology

2.1. Data acquisition

In this work, we used a statistical study of broken cells showing different crack types. Several test measurements are carried out on two different PV plants at the University of Huddersfield, United Kingdom. The first system consists of 10 polycrystalline PV modules with an optimum power 220 Wp. However, the second system consists of 35 polycrystalline with 130 Wp each. Both systems are shown in Fig. 1.

As presented in Fig. 1(a) and (b), there are two examined PV systems with a total amount of PV modules equal to 45. To establish the connection for each PV module separately, a controlling unit is designed to allow the user to connect any PV module to a FLEXmax 80 MPPT. In order to facilitate a real-time monitoring for each PV module, therefore, Vantage Pro monitoring unit is used to receive the Global solar irradiance measured by Davis weather station which includes pyranometer. Hub 4 communication manager is used to facilitate the acquisition of modules temperature using Davis external temperature sensor, and the electrical data for each photovoltaic module. LabVIEW software is used to implement the data logging and monitoring functions of the examined PV modules.

Fig. 1(c) shows the data acquisition system. Furthermore, Table 1 illustrates both electrical characteristics of the solar modules that are used in this work. The standard test condition (STC) for all examined solar panels are: Solar Irradiance = 1000 W/m²; Module Temperature = 25 °C.

2.2. Electroluminescence setup and PV modules cracks

The electroluminescence system developed is presented in Fig. 2(a). The system is comprised of a light-tight black-box where housed inside is a digital camera and a sample holder. The digital camera is equipped with a standard F-mount 18–55 mm lens. To allow for detection in the near infrared, the IR filter was removed and replaced with a full spectrum window of equal optical path length. In our setup, a Nikon D40 was used, but in principle, any digital camera with similar grade CCD or CMOS sensor and where

Fig. 1. (a) 10 PV Modules (SMT 6 (60) P) with 220 W Output Peak Power; (b) 35 PV Modules (KC130 GHT-2) with 130 W Output Peak Power; (c) Monitoring the Examined PV System Using LabVIEW Software.
the IR filter can be removed would serve the purpose. While the bias was applied, the resultant current and the voltage are measured by voltage and current sensors, which are wirelessly connected to a personal computer (PC). The purpose of the PC is to get the electroluminescence image of the solar module predicting the theoretical output power performance of the PV module.

In order to reduce the noise and increase the accuracy, all EL images are processed by removing background noise and erroneous pixels. Firstly, background image has been captured under the same conditions as the EL images but without forward biasing the cell. This background image is subtracted from each EL image in order to reduce the image noise level. The images are cropped to the appropriate size and in the case of high resolution imaging system, the captured cell images are compiled together to form an image of the entire module. Additionally, to increase the accuracy and the vision of the EL image, each PV module cell is captured separately.

In order to determine the cracks location, type and size; reflex camera has been used for imaging possible cracks in each PV module. As already explained, the EL imaging technique has been used worldwide and demonstrated by many researchers [14–16]. Broken cells are sorted according to the type of crack, Fig. 2 shows all examined crack types which are classified as follows:

A. Diagonal crack (+45°)
B. Diagonal crack (−45°)
C. Parallel to busbars crack
D. Perpendicular to busbars crack
E. Multiple directions crack

2.3. Theoretical output power modeling

The DC-Side for all examined PV modules is modeled using 5-parameters model. The voltage and the current characteristics of the PV module can be obtained using the single diode model [19] as the following:

\[ I = I_{ph} - I_0 \left( \frac{V_{ph}}{V_{ref}} - 1 \right) - \left( \frac{V + IR_s}{R_{sh}} \right) \]  

(1)

where \( I_{ph} \) is the photo-generated current at STC, \( I_0 \) is the dark saturation current at STC, \( R_s \) is the module series resistance, \( R_{sh} \) is the panel parallel resistance, \( n_s \) is the number of series cells in the PV module and \( V_t \) is the thermal voltage and it can be defined based on:

\[ V_t = \frac{AKT}{q} \]  

(2)

where \( A \) is the diode ideality factor, \( k \) is Boltzmann’s constant and \( q \) is the charge of the electron.

The five parameters are determined by solving the transcendental Equation (1) using Newton–Raphson algorithm. Based only

Table 1

<table>
<thead>
<tr>
<th>Solar panel electrical characteristics</th>
<th>1st system: PV module, SMT 6 (60)</th>
<th>2nd system: PV module, KC130 GHT-2</th>
</tr>
</thead>
<tbody>
<tr>
<td>Peak power (W)</td>
<td>220</td>
<td>130</td>
</tr>
<tr>
<td>Voltage at maximum power point (V_{mp})</td>
<td>28.7 V</td>
<td>17.6 V</td>
</tr>
<tr>
<td>Current at maximum power point (I_{mp})</td>
<td>7.67 A</td>
<td>7.39 A</td>
</tr>
<tr>
<td>Open circuit voltage (V_{oc})</td>
<td>36.7 V</td>
<td>21.9 V</td>
</tr>
<tr>
<td>Short circuit current (I_{sc})</td>
<td>8.24 A</td>
<td>8.02 A</td>
</tr>
<tr>
<td>Number of cells connected in series</td>
<td>60</td>
<td>36</td>
</tr>
<tr>
<td>Number of cells connected in parallel</td>
<td>1</td>
<td>1</td>
</tr>
<tr>
<td>PV system tilt angle and azimuth angle (North–South)</td>
<td>42°, 185°</td>
<td>42°, 180°</td>
</tr>
<tr>
<td>Davis pyranometer sensor tilt angle and azimuth angles (North–South)</td>
<td>42°, 185°</td>
<td>42°, 180°</td>
</tr>
</tbody>
</table>

Fig. 2. EL experimental setup and examined crack types. (a) Electroluminescence experimental setup; (b) Diagonal crack (+45°); (c) Diagonal crack (−45°); (d) Parallel to busbars crack; (e) Perpendicular to busbars crack; (f) Multiple directions crack.
on the datasheet of the available parameters shown previously in Table 1. The power produced by PV module in watts can be easily calculated along with the current (I) and voltage (V) that is generated by Equation (1), therefore, $P_{\text{theoretical}} = IV$.

2.4. Statistical analysis approach

After examining all PV modules which have cracks, a real time simulation can be processed. A statistical analysis approach is used to determine whether the PV crack has a significant impact on the total generated output power performance or not. Two statistical methods are used, T-test and F-test. The first method (T-test) is used to compare the simulated theoretical power with the measured PV output power. T-test can be evaluated using (3) where $\bar{x}$ is the mean of the samples, $\mu$ is the population mean, $n$ is the sample size and $SD$ is the standard deviation of the entire data.

In this work, we have used a confidence interval for all measured samples equal to 99%. Statistically speaking, the crack does not have a significant impact on the output power performance if the t-test value is significant, which means that the t-test value is less than or equal to 2.58 as shown in Table 2.

If the t-test value is not significant, another statistical method/layer is used to compare the output measured power from the cracked PV module with a PV module that has 0% of cracks. This layer is used to confirm that the output generated power of the cracked PV module has a significant impact (real damage) on the total generated output power performance of the examined photovoltaic module. In Section 4 (results section), most of the inspected results indicates that if the T-test value is significant, F-test value is also significant. The overall statistical approach can be explained in Fig. 3 and F-test can be evaluated using (4).

Table 2 illustrates the expected output results from F-test using a 99% ($P = 0.01$) confidence interval. In this work, an infinite number of samples (Total measured samples $> 120$) is used to determine whether the F-test value is significant (F-test $\leq 6.635$) or not significant (F-test $> 6.635$).

### 3. Results

3.1. Cracks distribution

As described previously, the statistic micro cracks location, type and size were established by taking EL images of 45 PV modules. The EL images were taken with a reflex camera [21]. From the captured pictures, the number of cracked cells in each module is counted as shown in Fig. 4.

<table>
<thead>
<tr>
<th>Degree of freedom (measured samples)</th>
<th>Output F-test for a significant results</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>4052.181</td>
</tr>
<tr>
<td>120</td>
<td>4.787</td>
</tr>
<tr>
<td>$\infty$</td>
<td>6.635</td>
</tr>
</tbody>
</table>

Table 3 illustrates the expected output results from F-test using a 99% ($P = 0.01$) confidence interval. In this work, an infinite number of samples (Total measured samples $> 120$) is used to determine whether the F-test value is significant (F-test $\leq 6.635$) or not significant (F-test $> 6.635$).

3. Results

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![Statistical approach used to identify whether the crack type has a significant impact on the output power performance of a photovoltaic module.](image-url)
Broken cells are sorted according to the type of crack they show and the classification already presented in Fig. 2. The probability for a cell to be cracked and the crack-type distribution are presented in Fig. 4. Only 15.556% of the total PV modules have no cracks. However, 84.444% of the PV modules contains at least one type of the crack: diagonal (26.666%), parallel to busbars (20%), perpendicular to busbars (8.888%) or multiple directions crack (28.888%).

According to the statistical approach explained previously in Fig. 3, T-test and F-test methods are significant based on a threshold values. Therefore, we have divided all crack-types into two main categories:

- Short: Crack affects one solar cell in a PV module
- Long: Crack affects two or more solar cells in a PV module

Furthermore, fitted line regression is used for the entire measured PV crack-type data. A fitted regression represents a mathematical regression equation for the PV measured data. We have selected the fitted regression lines to illustrate the relationship between a predictor variable (Measured PV Power) and a response variable (Irradiance Level) and to evaluate whether the model fits the data. If the measured PV power data is very close to the fitted line regression model, therefore, there is a significant relationship between the predictor with the response variable.

### 3.2 Diagonal cracks

Diagonal cracks can be classified into two different categories: +45° and −45° as shown in Fig. 2(a) and (b), respectively. The measured data taken from both diagonal crack categories indicate that there is a huge similarity in the measured output power performance for all PV modules examined. Therefore, we have classified both categories in one crack type. This result is different from those explained in [7,8] because all the measured data in our experiments were taken from a real-time long-term environmental measurement instead of laboratory climate conditions.

Using the statistical approach, the T-test values for all the examined diagonal crack PV modules (12 PV modules) are shown in Table 4. Since the T-test value for a diagonal crack affecting 1 or 2 solar cells is less than 99% of the confidence interval threshold (2.58), the output power performance for the PV module is statistically not significant. There is no evidence for a real damage in the PV module. The F-test for a diagonal crack affecting 1 or 2 solar cells is equal to 4.55 and 5.67, respectively. The mathematical expressions for the fitted line regression are illustrated in Table 4.

The real-time long-term measured data for a full day was carried out to estimate the output power performance for a diagonal crack affecting 1 and 5 solar cells are presented in Fig. 5(a).

<table>
<thead>
<tr>
<th>Table 4</th>
<th>Diagonal cracks performance indicators.</th>
</tr>
</thead>
<tbody>
<tr>
<td>Diagonal crack</td>
<td>Number of effected solar cells</td>
</tr>
<tr>
<td>Short +45° OR Short −45°</td>
<td>1</td>
</tr>
<tr>
<td>Long +45° OR Long −45°</td>
<td>2</td>
</tr>
<tr>
<td>OR</td>
<td>3</td>
</tr>
<tr>
<td>OR</td>
<td>4</td>
</tr>
<tr>
<td>OR</td>
<td>5</td>
</tr>
</tbody>
</table>
theoretically simulated output power, which has been calculated using LabVIEW software, has a standard deviation of 61.46 which is very close to that for a diagonal crack affecting 1 solar cell (SD = 61.38). However, a diagonal crack affecting 5 solar cells has a huge reduction in the output power performance of the PV module where the standard deviation is equal to 60.99. Finally, the measured output power of the PV module matches the theoretical output power, therefore, the theoretical power in Fig. 5(a) cannot be seen. The same has been found in Figs. 6(a), 7(a) and 8(a).

Fig. 5(b) describes the output power efficiency for the examined diagonal cracks affecting 1, 2, 3, 4 and 5 solar cells. Between 0.35 and 0.44% reduction of power is estimated for a diagonal crack that affected 1 solar cell. However, the estimated reduction of power for a diagonal crack that affected 5 solar cells is between 2.97 and 5.37%. The output power efficiency can be estimated using (5).

3.3. Parallel to busbars cracks

As shown previously in Fig. 5, the parallel to the busbars cracks have a percentage of occurrence 20% (9 PV modules out of 45 examined PV modules) and they are listed as follows:

- 8.888% (4 PV modules): Short Crack Effect
- 11.111% (5 PV modules): Long Crack Effect

Not all parallel to busbars cracks have a significant impact/reduction on the output power performance of the PV module. As shown in Table 5, the parallel to busbars crack affecting 1 solar cell statistically indicates that there is no real damage in the PV module, the result is confirmed by the T-test value which is less than the threshold value 2.58. Moreover, when the parallel to busbars crack affecting 2 solar cells with an approximate broken area of less than 82 mm² has no significant effect on the amount of power generated by the PV module. Additionally, Table 5 illustrates various mathematical equations for the measured fitted line regression which describes the relationship between the theoretically calculated and measured output powers.

Fig. 6(a) presents the real-time measured data for a parallel to busbars crack affecting 1 and 4 solar cells. The standard deviation for the theoretically simulated power is 62.01, which is very close to the standard deviation for a parallel to busbars crack affecting 1 solar cell (61.8). However, the parallel to busbars crack affecting 5 solar cells has a huge reduction in the output power performance of the PV module while the standard deviation is equal to 61.09.

Fig. 6(b) describes the output power efficiency for the examined parallel to busbars cracks affecting 1, 2, 3 and 4 solar cells. The reduction of power estimated for a parallel to busbars crack affecting 1 solar cell is between 0.75% and 0.97%. However, the estimated reduction of power for a parallel to busbars crack affecting 3 and 4 solar cells is between 2.39%–3.0% and 3.67%–4.55%, respectively.
Efficiency = \frac{\text{Measured Output Power}}{\text{Theoretical Output Power}} \times 100\% \quad (5)

3.4. Perpendicular to busbars cracks

Perpendicular to busbars cracks usually do not occur in PV modules. In research have distinguished only 4 PV modules from 45 to be classified as a perpendicular to busbars cracks. This result has been verified by many articles such as [7,8]. Table 6 shows all numerical results which are measured from the examined PV modules.

Table 6 indicates that perpendicular to busbars crack effects 1, 2 and 3 busbars statistically have no significant impact on the overall amount of power produced by a PV module. The measured results for a perpendicular to busbars cracks effects 1 and 4 solar cells can be seen in Fig. 7(a), the difference between the theoretical standard deviation and a perpendicular to busbars cracks which effects 4 solar cells is equal to 1.014. Finally, Fig. 7(b) illustrates the output power efficiency measured for a perpendicular to busbars which effects 1, 2, 3 and 4 solar cells (1~8 Busbars), where the maximum power reduction is estimated for 8 busbars between 4.6 and 4.1%.

3.5. Multiple directions crack

Multiple directions cracks have the highest degradation in the PV measured output power. Three different measured data are presented in Fig. 8(a). As illustrated in Fig. 8(b), the multiple directions crack affected 5 solar cells, reducing the power efficiency of the PV module up to 8.42%. However, the average reduction in the power for the multiple directions crack affecting 1 solar cell with an approximate broken area of less than 46.2 mm² is equal to 1.04%.

Table 7 shows a brief explanation for the T-test values and whether a multiple directions crack has a significant or not significant impact on the total output power produced by a cracked PV module.

4. Discussion

4.1. Overall cracks assessment

The observed modules have 38 PV modules with various crack types. The probability of occurrence for each crack type can be seen in Fig. 4. Before considering the statistical approach, it is hypothetically true to say that 84.4% has a significant impact on the output power performance. However, the statistical approach has confirmed that this is incorrect, because only 60% has a significant impact on the output power performance for all PV modules examined.

This result can be investigated further by applying the same statistical approach on various PV systems in different regions around the world. The only difference might be the confidence interval limitations (99%, 95% and 90%) due to the various accuracy rates for the instrumentation used in the PV systems such as the Voltage sensors, Current sensors, and Temperature sensors (Fig. 9).
4.2. Surface damage

For better understanding how some cracks affect the surface of the PV modules, we have created a MATLAB code which can simulate the measured data of a cracked PV module in order to evaluate the surface shape for a particular crack-type using Surf(x, y, z) MATLAB function [22].

Fig. 10(a) shows a diagonal crack (45°) that affected 3 solar cells. It is clear that the surfaces of these three different solar cells are damaged (Noted as 1, 2 and 3). The degradation of the power for the solar cells is between 0.5 and 1 Watt. The overall PV module efficiency can be estimated by the MATLAB code which is equal to 98.61%, as illustrated in Figs. 5(b) and 10(a).

Similarly, Fig. 10(b) describes the surface shape of a parallel to busbars crack which affects 3 solar cells. The degradation of the power in the affected solar cells is between 2.5 and 2 Watt. The overall power efficiency of the PV module is equal to 97.41% which is very similar to the value (97.4%) described earlier in Fig. 6(b).

The surface shape for a perpendicular to busbars crack affecting 3 solar cells, 6 Busbars is illustrated in Fig. 10(c). Overall efficiency of the cracked surfaces is equal to 97.28% for a perpendicular to busbars crack which affects 3 solar cells (6 busbars), and 95.3% for a multiple directions crack which affects 3 solar cells.

The surface shape for a perpendicular to busbars crack affecting 3 solar cells, 6 Busbars is illustrated in Fig. 10(c). However, Fig. 10(d) shows a cracked surface for a PV module that is affected by a multiple directions crack on 3 different solar cells. Moreover, a perpendicular crack effect solar cell with 2 busbars has an estimated degradation of power equals to 1.5 Watt.

5. Conclusion

This paper proposes a new statistical algorithm to identify the significant effect of cracks on the output power performance of the PV modules. The algorithm is developed using a Virtual Instrumentation (VI) LabVIEW software. We have examined 45 PV modules with various types of crack such as diagonal, parallel to busbars, perpendicular to busbars and multiple directions cracks.

Before considering the statistical approach, 84.44% of the examined PV modules have a significant impact on the output power performance. However, the statistical approach has confirmed that this result is incorrect, since only 60% of the examined PV cracks have a significant impact on the output power performance.

Based on the measured output power data of each crack-type PV module, we have evaluated the fitted line regression equations. Subsequently, the surfaces of cracked PV modules have been demonstrated using Surf(x, y, z) MATLAB Function.
Fig. 8. (a) Real-time long-term measured data for a multiple directions crack effect on 1, 3 and 5 solar cells; (b) Output power efficiency for a multiple directions crack affecting 1,2,3,4 and 5 PV solar cells.

Fig. 9. Percentage of cracks in the examined PV modules, overall significant cracks equal to 60% out of 84.444%.
Table 5
Parallel to busbars cracks performance indicators.

<table>
<thead>
<tr>
<th>Crack type</th>
<th>Number of effected solar cells</th>
<th>Approximate area broken (mm)</th>
<th>T-test value</th>
<th>Significant/Not significant effect on the PV power performance</th>
<th>Fitted line regression equation</th>
</tr>
</thead>
<tbody>
<tr>
<td>Parallel to busbars</td>
<td>Short</td>
<td>1</td>
<td>1 mm²–59.2 mm²</td>
<td>0.78–1.13</td>
<td><strong>Not significant</strong></td>
</tr>
<tr>
<td></td>
<td>Long</td>
<td>2</td>
<td>63 mm²–81 mm²</td>
<td>1.42–1.87</td>
<td><strong>Not significant</strong></td>
</tr>
<tr>
<td></td>
<td></td>
<td>3</td>
<td>82 mm²–121 mm²</td>
<td>2.62–2.74</td>
<td>Significant</td>
</tr>
<tr>
<td></td>
<td></td>
<td>4</td>
<td>122 mm²–177 mm²</td>
<td>4.04–4.81</td>
<td>Significant</td>
</tr>
<tr>
<td></td>
<td></td>
<td>5</td>
<td>177.3 mm²–239.7 mm²</td>
<td>4.39–5.66</td>
<td>Significant</td>
</tr>
</tbody>
</table>

Table 6
Perpendicular to busbars cracks performance indicators.

<table>
<thead>
<tr>
<th>Crack type</th>
<th>Number of effected solar cells</th>
<th>Number of effected busbars</th>
<th>Approximate area broken (mm)</th>
<th>T-test value</th>
<th>Significant/Not significant effect on the PV power performance</th>
<th>Fitted line regression equation</th>
</tr>
</thead>
<tbody>
<tr>
<td>Perpendicular to busbars</td>
<td>Short</td>
<td>1</td>
<td>1</td>
<td>1 mm²–16.2 mm²</td>
<td>0.65–0.82</td>
<td><strong>Not significant</strong></td>
</tr>
<tr>
<td></td>
<td>2</td>
<td>16.3 mm²–80 mm²</td>
<td>0.92–1.31</td>
<td><strong>Not significant</strong></td>
<td>$P_{BH} = 0.1524 + 1.002P_{MEO}$</td>
<td></td>
</tr>
<tr>
<td></td>
<td>Long</td>
<td>3</td>
<td>61.3 mm²–78.5 mm²</td>
<td>1.43–1.96</td>
<td><strong>Not significant</strong></td>
<td>$P_{BH} = 0.3604 + 1.004P_{MEO}$</td>
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<tr>
<td></td>
<td></td>
<td>4</td>
<td>79.4 mm²–120 mm²</td>
<td>2.52–2.77</td>
<td>Significant</td>
<td>$P_{BH} = 0.4678 + 1.005P_{MEO}$</td>
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<tr>
<td></td>
<td></td>
<td>5</td>
<td>120.5 mm²–137.4 mm²</td>
<td>2.83–2.94</td>
<td>Significant</td>
<td>$P_{BH} = 0.7397 + 1.008P_{MEO}$</td>
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<td></td>
<td></td>
<td>6</td>
<td>138 mm²–179.8 mm²</td>
<td>2.79–3.11</td>
<td>Significant</td>
<td>$P_{BH} = 0.9265 + 1.010P_{MEO}$</td>
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<tr>
<td></td>
<td></td>
<td>4</td>
<td>181.5 mm²–195 mm²</td>
<td>3.02–3.27</td>
<td>Significant</td>
<td>$P_{BH} = 1.0790 + 1.012P_{MEO}$</td>
</tr>
<tr>
<td></td>
<td></td>
<td>8</td>
<td>196.2 mm²–240.2 mm²</td>
<td>3.19–3.55</td>
<td>Significant</td>
<td>$P_{BH} = 1.4590 + 1.018P_{MEO}$</td>
</tr>
</tbody>
</table>

Table 7
Multiple directions cracks performance indicators.

<table>
<thead>
<tr>
<th>Crack type</th>
<th>Number of effected solar cells</th>
<th>Approximate area broken (mm)</th>
<th>T-test value</th>
<th>Significant/Not significant effect on the PV power performance</th>
<th>Fitted line regression equation</th>
</tr>
</thead>
<tbody>
<tr>
<td>Multiple directions crack</td>
<td>1</td>
<td>1</td>
<td>1 mm²–45 mm²</td>
<td>2.06–2.44</td>
<td><strong>Not significant</strong></td>
</tr>
<tr>
<td></td>
<td>2</td>
<td>46.2 mm²–1000 mm²</td>
<td>2.68–2.88</td>
<td>Significant</td>
<td>$P_{BH} = 0.5330 + 1.005P_{MEO}$</td>
</tr>
<tr>
<td></td>
<td>3</td>
<td>100 mm²–3700 mm²</td>
<td>3.25–3.33</td>
<td>Significant</td>
<td>$P_{BH} = 1.028 + 1.012P_{MEO}$</td>
</tr>
<tr>
<td></td>
<td>4</td>
<td>170 mm²–5000 mm²</td>
<td>4.70–4.88</td>
<td>Significant</td>
<td>$P_{BH} = 1.554 + 1.019P_{MEO}$</td>
</tr>
<tr>
<td></td>
<td>5</td>
<td>223 mm²–8200 mm²</td>
<td>6.17–6.31</td>
<td>Significant</td>
<td>$P_{BH} = 2.015 + 1.027P_{MEO}$</td>
</tr>
<tr>
<td></td>
<td>6</td>
<td>400 mm²–9800 mm²</td>
<td>7.30–7.52</td>
<td>Significant</td>
<td>$P_{BH} = 2.577 + 1.033P_{MEO}$</td>
</tr>
</tbody>
</table>

Fig. 10. (a) Surface shape for a diagonal (–45°) crack effect 3 solar cells; (b) Surface shape for a parallel to busbars crack effect 3 solar cells (c) Surface shape for a perpendicular to busbars crack effect 3 solar cells, 6 busbars; (d) Surface shape for a multiple directions crack effect 3 solar cells.
For further work, we are designing a generic algorithm based on statically analysis techniques to detect multiple faults in PV systems such as DC-Side faults, AC-Side faults, PV cracks and shading effect.

Acknowledgments

The authors would like to acknowledge financial support from the University of Huddersfield, Engineering and Computing Department.

References